

# IT4PQ Final Stakeholder Workshop



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## Simplified test procedures for frequency characterization of inductive VTs

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IT4PQ Final Workshop

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degli Studi  
della Campania  
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# Acknowledgement



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# Simplified Procedures: Target

Characterize Inductive MV VT For Harmonics Measurement  
Currently, two main approaches are adopted:

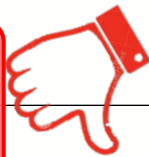
## APPROACH A

VTs frequency response is evaluated by carrying out a sinusoidal frequency sweep (SFS) at LV

EASY,  
AFFORDABLE



LESS  
ACCURATE



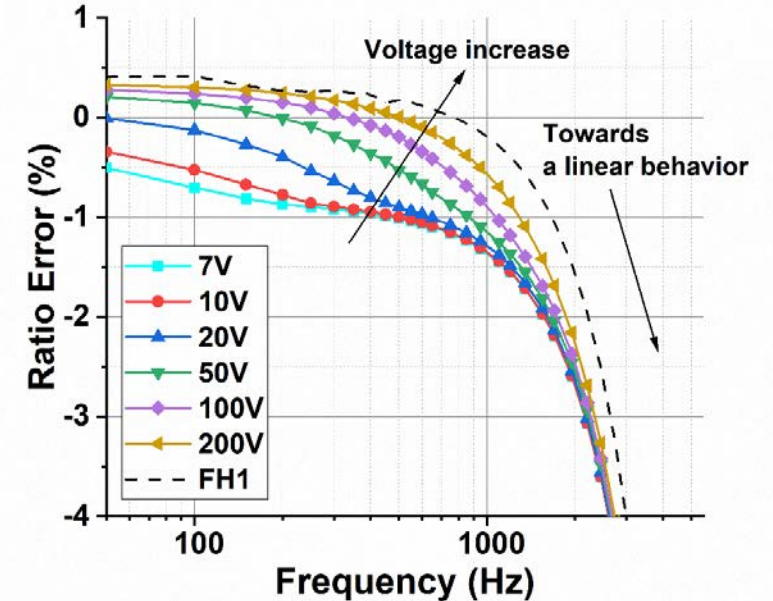
## APPROACH B

VTs frequency response is evaluated under non-standardized waveforms such as bi-tone (FH1) or multi-tone signals (FHN) at MV.

ACCURATE



EXPENSIVE  
SETUP



*When a VT is supplied at LV, the magnetization of the iron-core is low compared with the magnetization obtained at rated operating point.*

# Simplified Procedures: Description

## NEW PROPOSED APPROACH: 2-STEPS PROCEDURE FOR VTs FREQUENCY RESPONSE MEASUREMENT

### STEP 1

Measurement of the VT:

- errors at power frequency and rated amplitude

$$(\epsilon_{50 \text{ Hz}}, \Delta\varphi_{50 \text{ Hz}})$$

- first 10-15 harmonic spurious tones

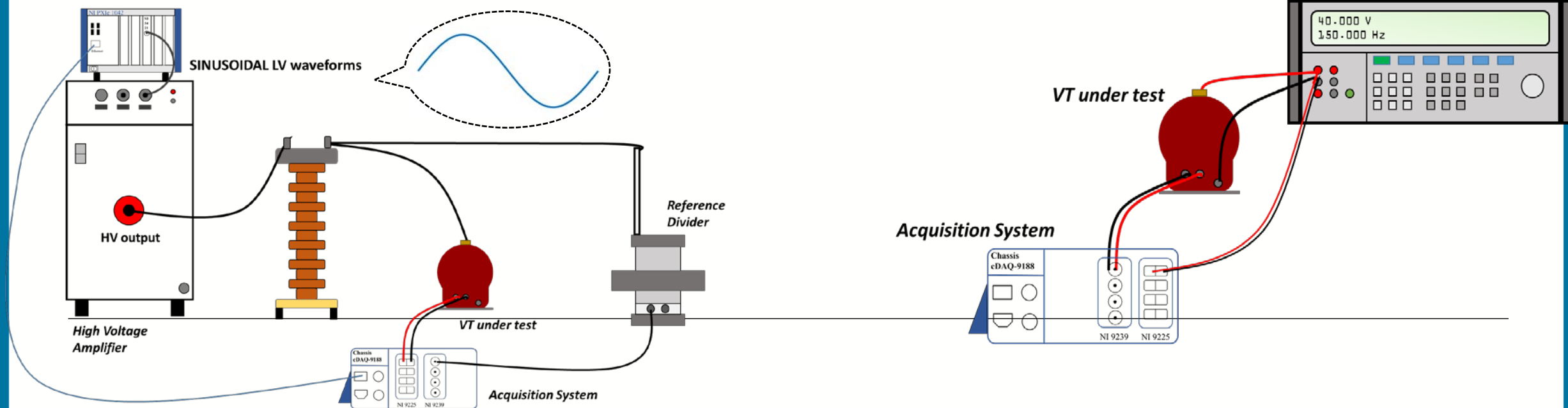
### STEP 2

Measurement of the VT:

- harmonics errors under a LV SFS

$$\epsilon_h = \frac{k_r V_{s,h} - V_{p,h}}{V_{p,h}}$$

$$\Delta\varphi_h = \varphi_{s,h} - \varphi_{p,h}$$



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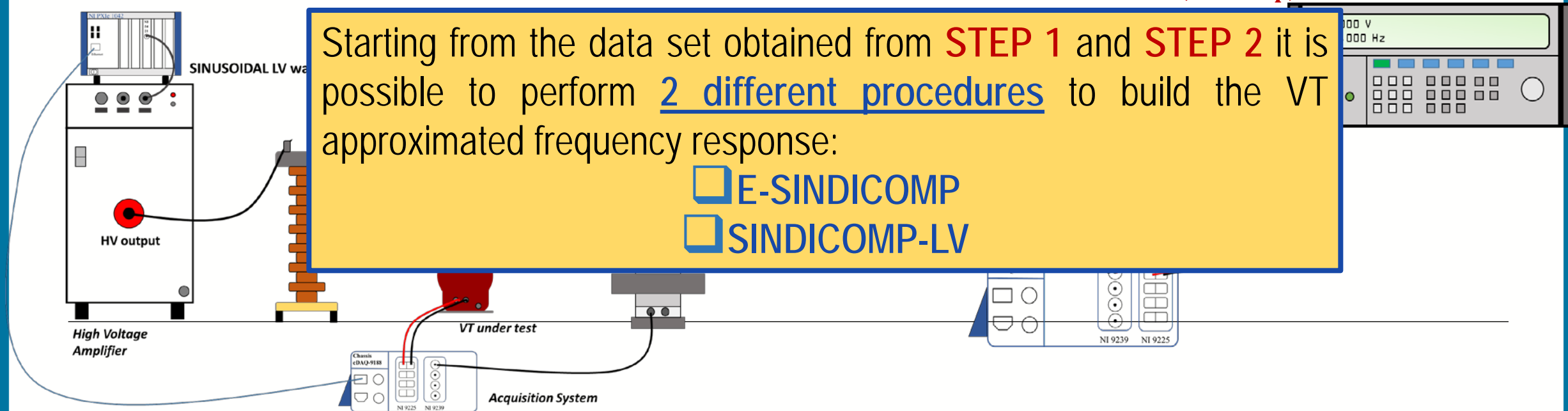
- harmonics errors under a LV SFS

$$\epsilon_h = \frac{k_r V_{s,h} - V_{p,h}}{V_{p,h}}$$

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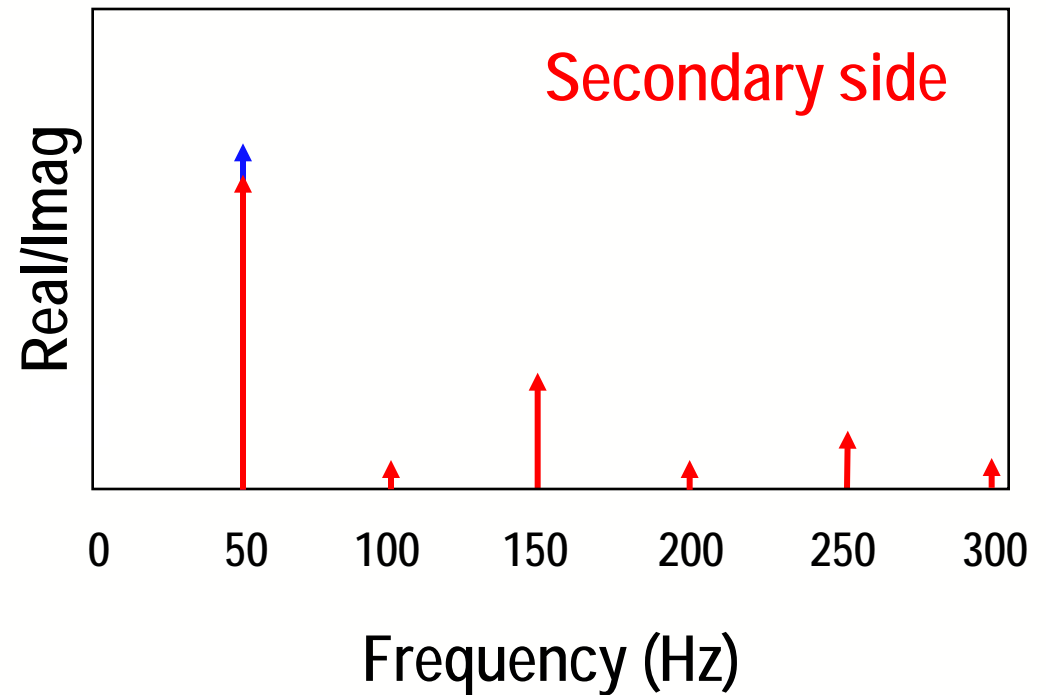
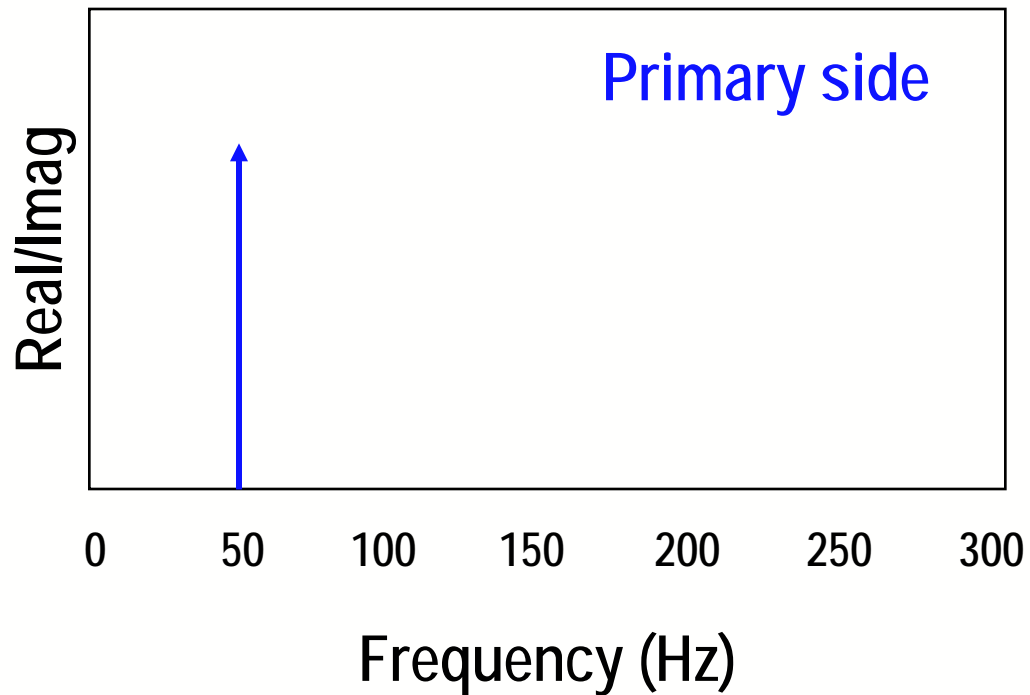
Starting from the data set obtained from **STEP 1** and **STEP 2** it is possible to perform 2 different procedures to build the VT approximated frequency response:

- E-SINDICOMP
- SINDICOMP-LV



# E-SINDICOMP and SINDICOMP-LV: Preliminary Step (1/2)

Shared Preliminary Step: Non Linearity Compensation

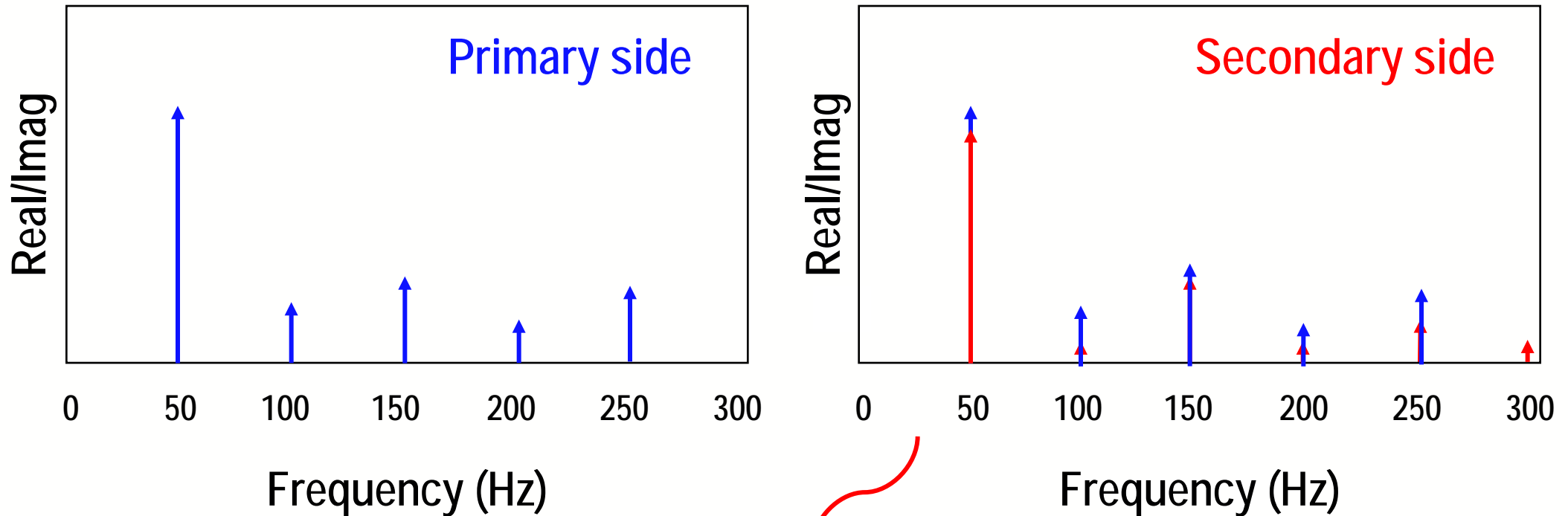


**Harmonic Distortion** ⇒

Spurious harmonic generated by the fundamental tone because of the B-H curve non-linearity of the VT.

# E-SINDICOMP and SINDICOMP-LV: Preliminary Step (1/2)

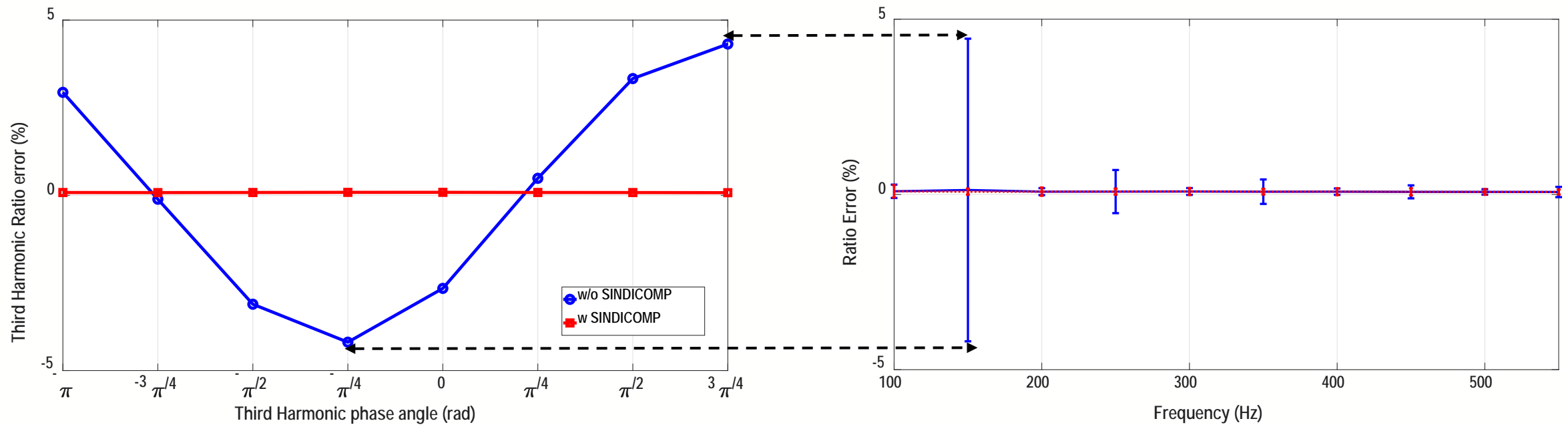
Shared Preliminary Step: Non Linearity Compensation



Combination of the harmonic applied to the input of the VT and the spurious harmonic generated by the fundamental.

# E-SINDICOMP and SINDICOMP-LV: Preliminary Step (2/2)

## SINDICOMP: SINusoidal characterization for DIstortion COMPensation



$U_h = 1\%$  of rated voltage

More information: A. Cataliotti et al., "Compensation of Nonlinearity of Voltage and Current Instrument Transformers," in *IEEE Transactions on Instrumentation and Measurement*, vol. 68, no. 5, pp. 1322-1332, May 2019, doi: 10.1109/TIM.2018.2880060.

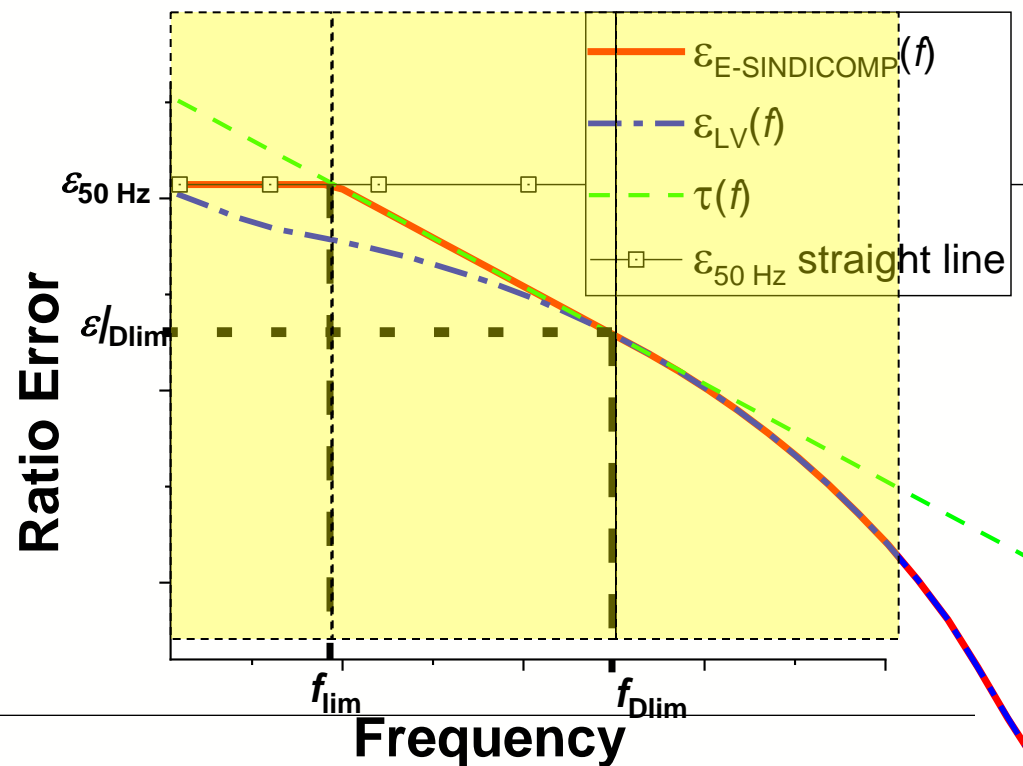
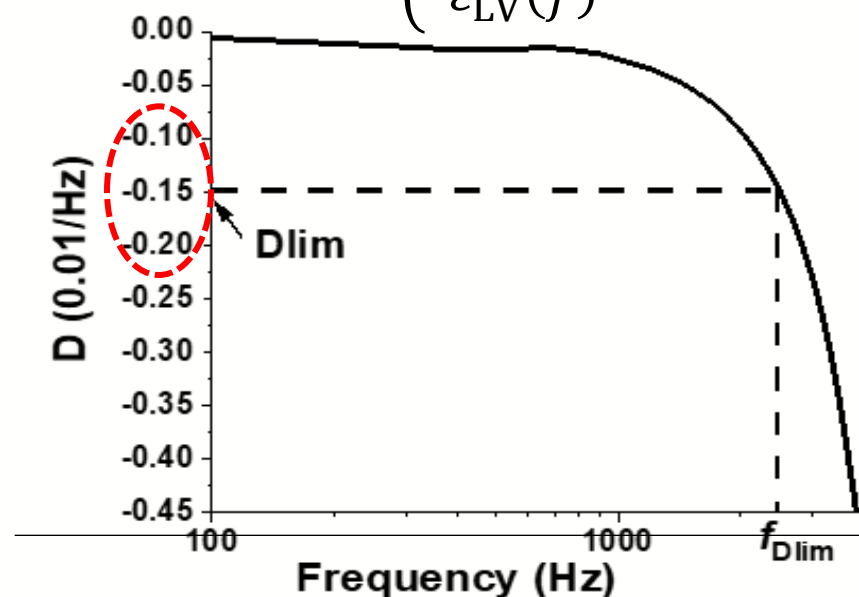


# E-SINDICOMP: Description

## APPROXIMATED RATIO ERROR FREQUENCY RESPONSE:

1. the VT ratio error at power frequency and rated amplitude  $\epsilon_{50\text{ Hz}}$
2. the low voltage frequency responses  $\epsilon_{LV}(f)$ ,
3. the  $\tau(f)$  curve obtained through the study of the derivative  $D$  of the low voltage frequency response  $\epsilon_{LV}(f)$ .

$$\epsilon_{E-SINDICOMP}(f) = \begin{cases} \epsilon_{50\text{ Hz}} & 50\text{ Hz} \leq f < f_{\text{lim}} \\ \tau(f) & f_{\text{lim}} \leq f < f_{\text{Dlim}} \\ \epsilon_{LV}(f) & f \geq f_{\text{Dlim}} \end{cases}$$



# SINDICOMP-LV: Description (1/2)

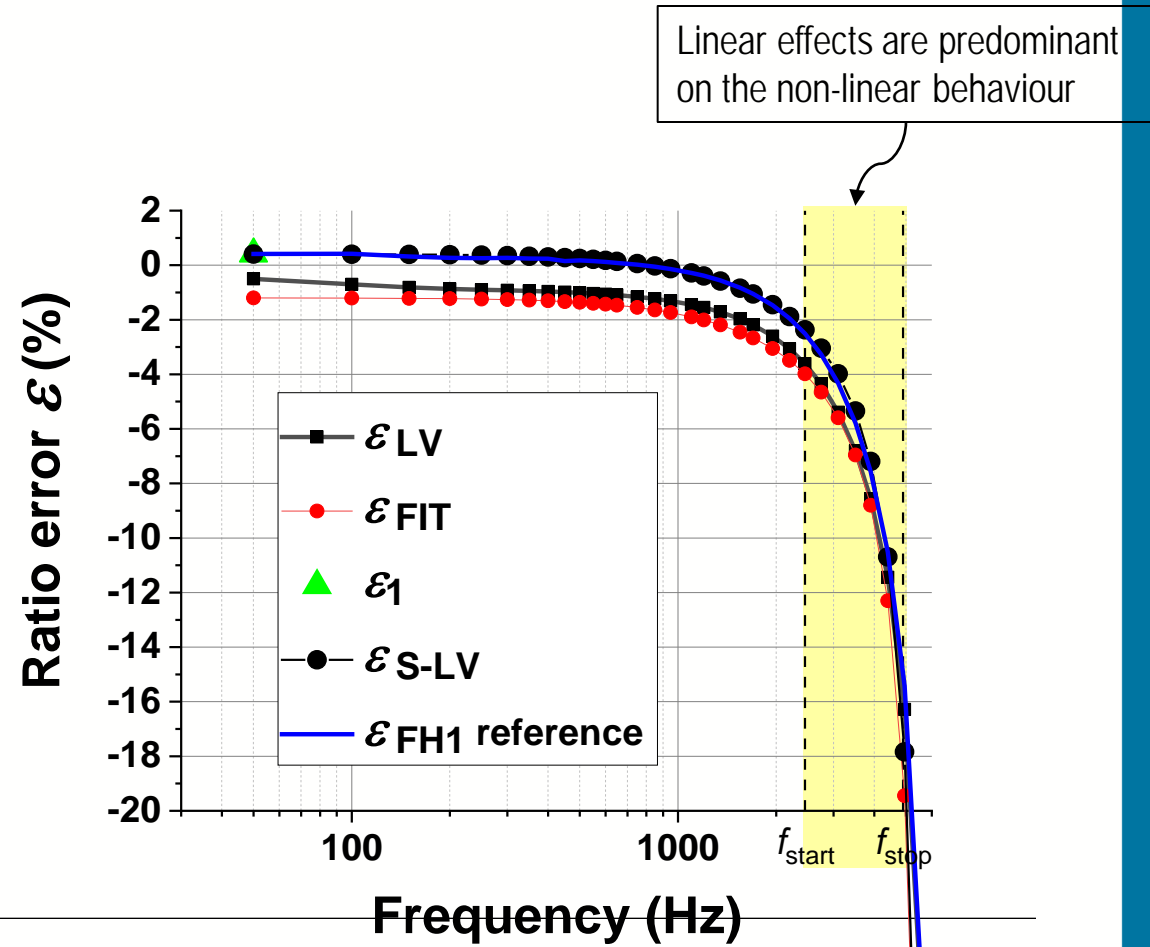
## APPROXIMATED RATIO ERROR FREQUENCY RESPONSE:

1. the low voltage frequency responses  $\varepsilon_{LV}(f)$  (■),
2. the  $\varepsilon_{FIT}(f)$  function (●)
3. the VT ratio error at rated frequency and rated amplitude  $\varepsilon_1$  (▲)

$$\varepsilon_{S-LV}(f) = \begin{cases} \varepsilon_{FIT}(f) + \varepsilon_{OFS,a} & f_1 \leq f < f_{start} \\ \varepsilon_{LV}(f) + \varepsilon_{OFS,b} & f_{start} \leq f < f_{stop} \end{cases}$$

$$\varepsilon_{FIT}(f) = \frac{\sqrt{(2\pi f a)^2 + b^2}}{\sqrt{\left(1 - \left(f/f_R\right)^2\right)^2 + \left(f/2\pi f_R^2 \cdot b/a\right)^2}}$$

$f_R$  is the first resonance frequency.



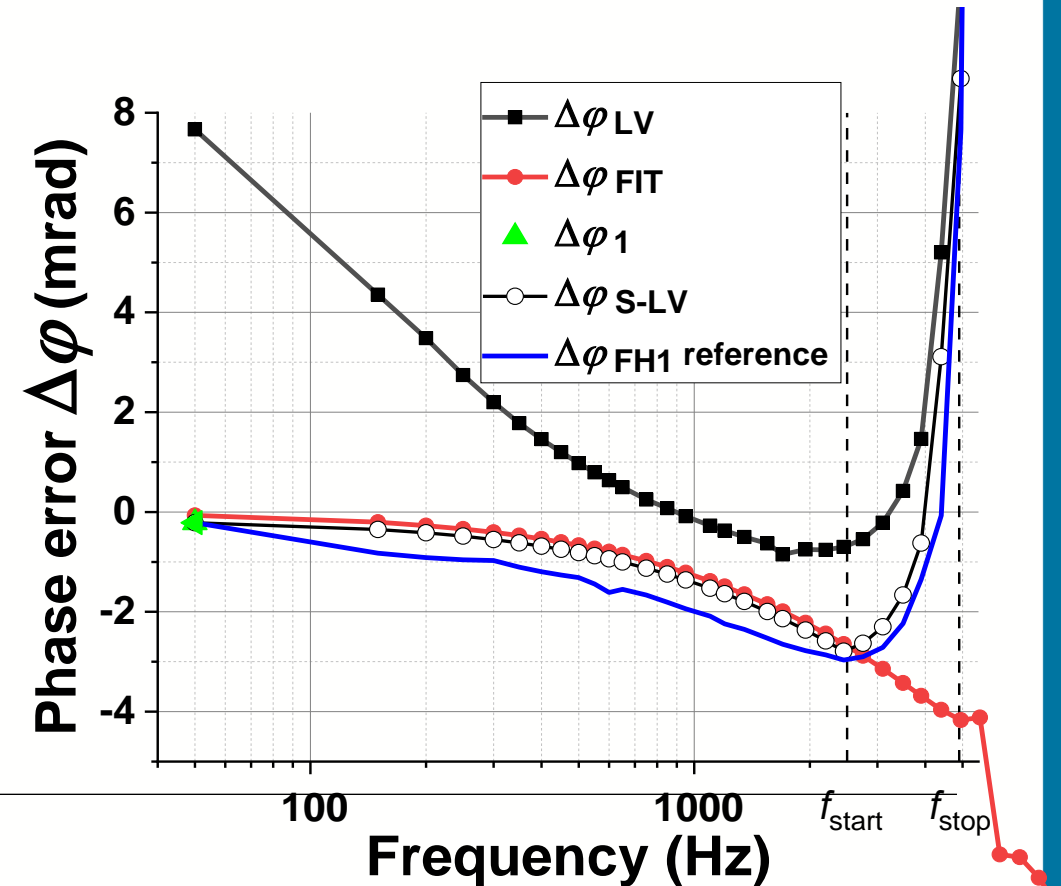
# SINDICOMP-LV: Description (2/2)

APPROXIMATED PHASE ERROR FREQUENCY RESPONSE:

1. the low voltage frequency responses  $\Delta\varphi_{LV}(f)$  (■)
2. the fit function with the parameter  $a$  and  $b$  found for the ratio error approximation (●)
3. the VT phase error at rated frequency and rated amplitude  $\Delta\varphi_1$  (▲)

$$\Delta\varphi_{S-LV}(f) = \begin{cases} \Delta\varphi_{FIT}(f) + \Delta\varphi_{OFS,a} & f_1 \leq f < f_{start} \\ \Delta\varphi_{LV}(f) + \Delta\varphi_{OFS,b} & f_{start} \leq f < f_{stop} \end{cases}$$

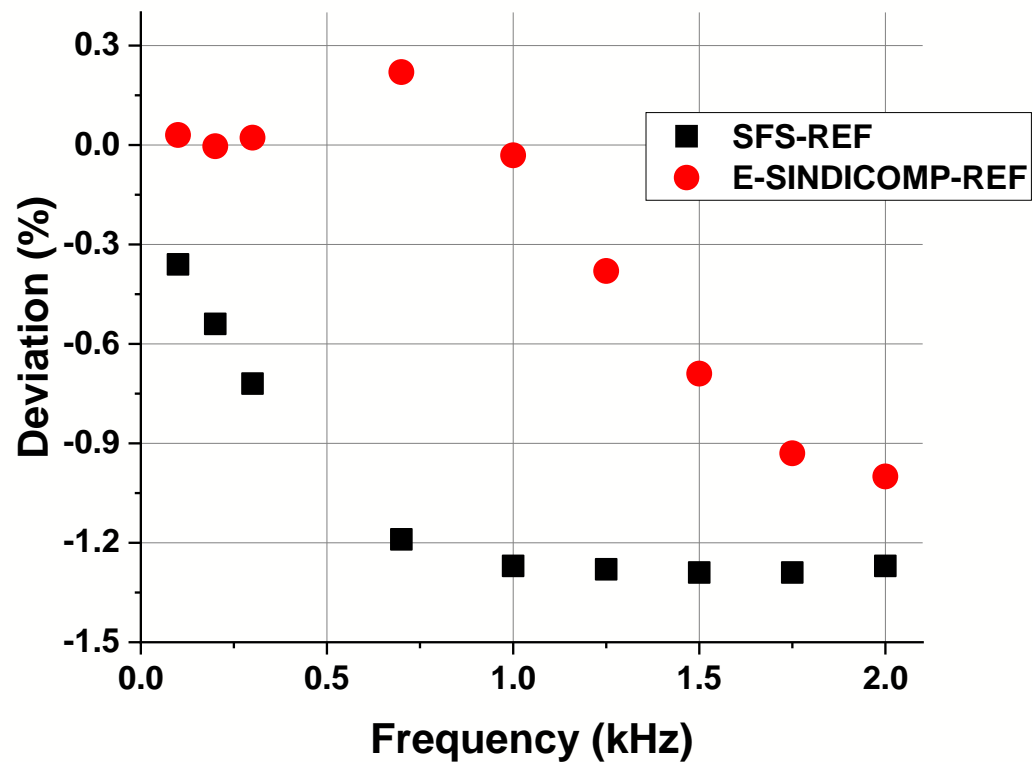
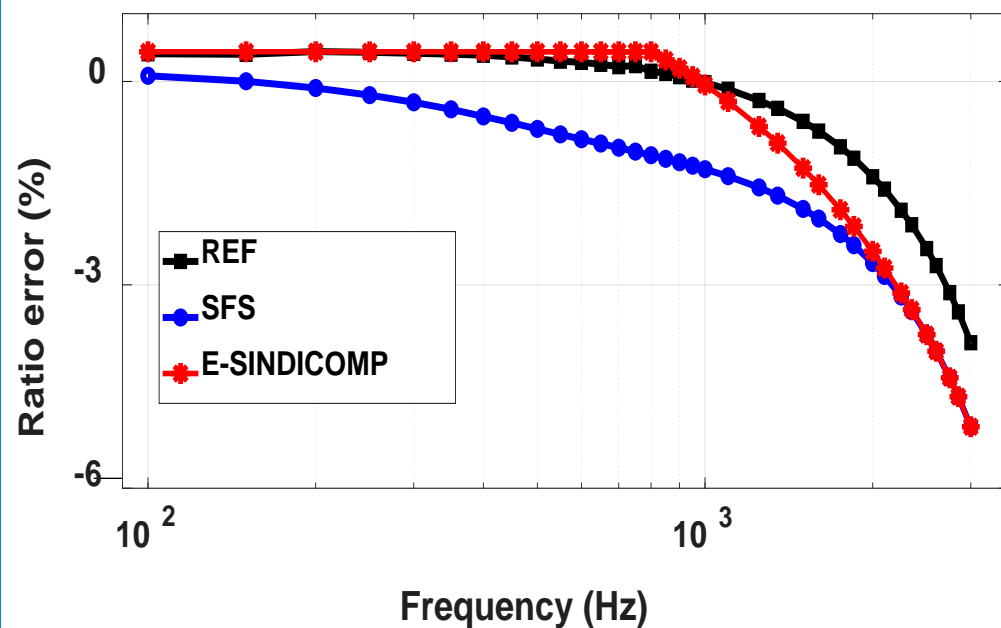
$$\varphi_{FIT}(f) = \arctan\left(2\pi f \cdot \frac{a}{b}\right) - \arctan\left(\frac{\frac{f}{2\pi f_R^2} \cdot \frac{b}{a}}{\left(1 - \left(\frac{f}{f_R}\right)^2\right)^2}\right) + 2\pi f \cdot \frac{a}{b}$$



# E-SINDICOMP: Application

- Device under test: MV inductive VT  
20/ $\sqrt{3}$  kV / 100 / $\sqrt{3}$  V; 30 VA; 0.5 accuracy class
- SFS at 40 V

$D_{lim}$ (0.01/Hz)	$f_{Dlim}$ (Hz)	$f_{lim}$ (Hz)
-0.15	2500	800



**@ 300 Hz: from -0.72 % to 0.02%**

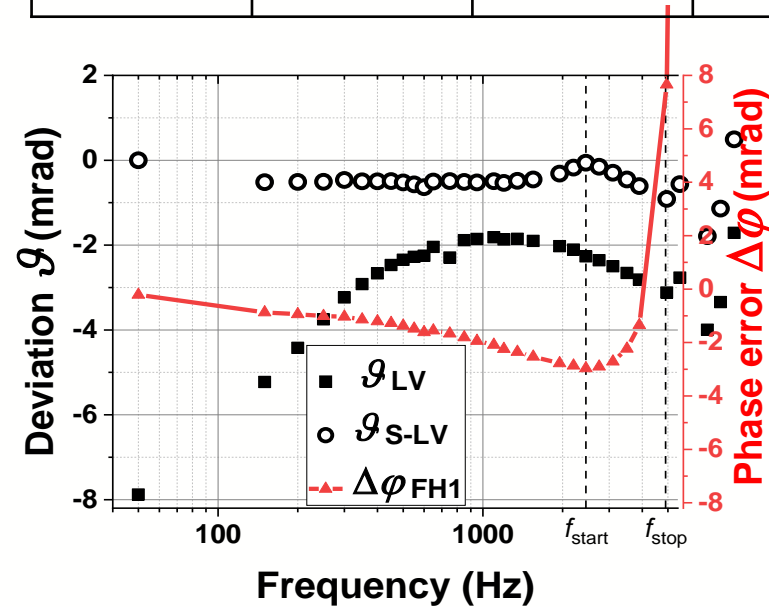
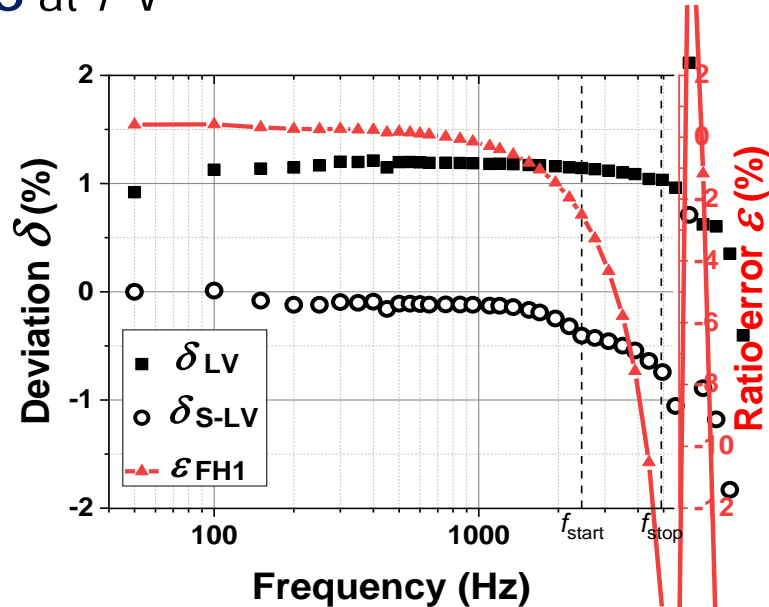
**@ 1 kHz: from 1.3 % to 0.03%**

**@ 2 kHz: from -1.27% to -1%**

# SINDICOMP-LV: Application

- Device under test: MV inductive VT  
20/ $\sqrt{3}$  kV / 100 / $\sqrt{3}$  V; 30 VA; 0.5 accuracy class
- SFS at 7 V

$f_R$ (Hz)	$f_{start}$ (Hz)	$f_{stop}$ (Hz)	$a$ (s)	$b$
5900	2450	4900	0.2	1.7



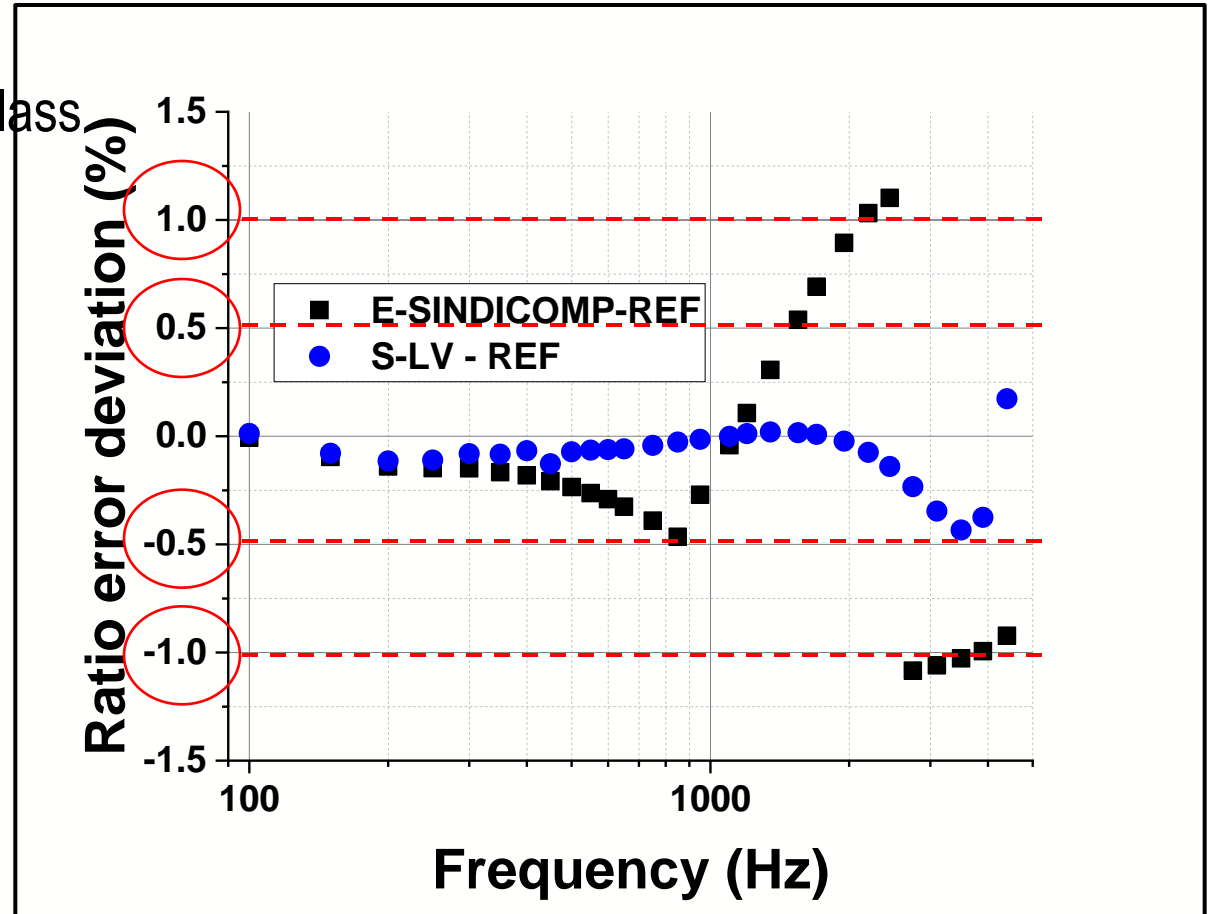
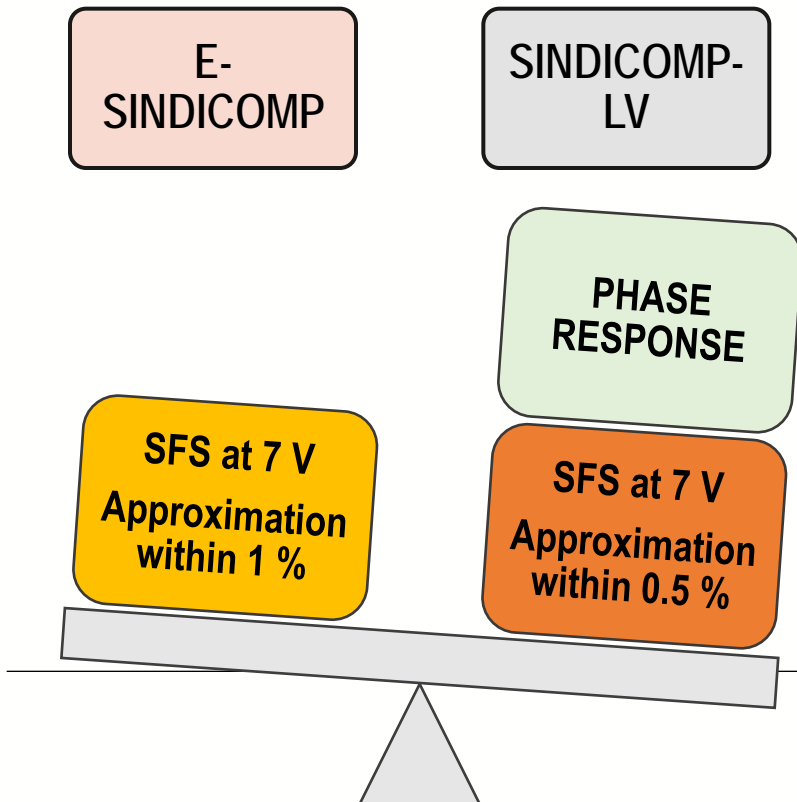
**@ 400 Hz: from -1.14 % to 0.08% and from -2.67 mrad to -0.5 mrad**

**@ 1.2 kHz: from 1.18 % to -0.10% and from -1.88 mrad to -0.54 mrad**

**@ 3.5 kHz: from 1.05 % to -0.43% and from -2.65 mrad to -0.58 mrad**

# E-SINDICOMP vs SINDICOMP-LV: Comparison among the two techniques

- Device under test: MV inductive VT  
20/ $\sqrt{3}$  kV / 100 / $\sqrt{3}$  V; 30 VA; 0.5 accuracy class
- SFS at 7 V



# Conclusion

- ✓ **Two** simplified procedures (**E-SINDICOMP** and **SINDICOMP-LV**) for the measurement of the frequency response of the MV VTs in common industrial laboratories.
  - ✓ The E-SINDICOMP technique provides a method for the only approximation of VT ratio error response whereas **SINDICOMP-LV allows to build the VT frequency response in terms of both amplitude and phase.**
  - ✓ The **simplified methods** have been applied for the frequency characterization of three different VTs and **validated by comparison with** results obtained using the **FH1 reference measurement method.**
  - ✓ Both the simplified procedures allow reaching an accuracy **improvement** with respect to the use of a conventional LV SFS technique **up to one order of magnitude for the ratio error.**
  - ✓ The results provided by the two simplified techniques are then compared with each other and it is found that **SINDICOMP-LV produces a better approximation** of the VT ratio error frequency response. In particular, SINDICOMP-LV accuracy performance in the VT ratio error evaluation is found within 0.4% up to 20<sup>th</sup> harmonic, and within 1% close to the resonance frequency; as to the phase error, it is always within 0.8 mrad.
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